ME:5160 (58:160) Intermediate Mechanics of Fluids

Fall 2024 – HW9 Solution

P6.39 By analogy with laminar shear, $\tau = \mu du/dy$. T. V. Boussinesq in 1877 postulated that turbulent shear could also be related to the mean-velocity gradient $\tau turb = \varepsilon du/dy$, where ε is called the *eddy viscosity* and is much larger than μ . If the logarithmic-overlap law, Eq. (6.28), is valid with $\tau \approx \tau w$, show that $\varepsilon \approx \kappa \rho u^* y$.

Solution: Differentiate the log-law, Eq. (6.28), to find du/dy, then introduce the eddy viscosity into the turbulent stress relation

If
$$\frac{u}{u^*} = \frac{1}{\kappa} \ln\left(\frac{yu^*}{v}\right) + B$$
, then $\frac{du}{dy} = \frac{u^*}{\kappa y}$
Then, if $\tau \approx \tau_w = \rho u^{*2} = \varepsilon \frac{du}{dy} = \varepsilon \frac{u^*}{\kappa y}$, solve for $\varepsilon = \kappa \rho u^* y$ Ans.

Note that $\varepsilon/\mu = \kappa y^+$, which is much larger than unity in the overlap region.

P6.40 Theodore von Kármán in 1930 theorized that turbulent shear could be represented by τ turb = ε du/dy where $\varepsilon = \rho \kappa^2 y^2 |$ du/dy | is called the *mixing-length eddy viscosity* and $\kappa \approx$ 0.41 is Kármán's dimensionless *mixing-length constant* [2,3]. Assuming that τ turb $\approx \tau w$ near the wall, show that this expression can be integrated to yield the logarithmic-overlap law, Eq. (6.28).

Solution: This is accomplished by straight substitution:

$$\tau_{\text{turb}} \approx \tau_{\text{w}} = \rho u^{*2} = \varepsilon \frac{\text{du}}{\text{dy}} = \left[\rho \kappa^2 y^2 \left| \frac{\text{du}}{\text{dy}} \right| \right] \frac{\text{du}}{\text{dy}}, \text{ solve for } \frac{\text{du}}{\text{dy}} = \frac{u^*}{\kappa y}$$

Integrate:
$$\int du = \frac{u^*}{\kappa} \int \frac{dy}{y}$$
, or: $u = \frac{u^*}{\kappa} \ln(y) + \text{constant}$ Ans.

To convert this to the exact form of Eq. (6.28) requires fitting to experimental data

P6.44 Mercury at 20°C flows through 4 meters of 7-mm-diameter glass tubing at an average velocity of 5 m/s. Estimate the head loss in meters and the pressure drop in kPa.

Solution: For mercury at 20°C, take $\rho = 13550 \text{ kg/m}^3$ and $\mu = 0.00156 \text{ kg/m} \cdot \text{s}$. Glass tubing is considered hydraulically "smooth," $\varepsilon/d = 0$. Compute the Reynolds number:

$$Re_{d} = \frac{\rho V d}{\mu} = \frac{13550(5)(0.007)}{0.00156} = 304,000; \text{ Moody chart smooth: } f \approx 0.0143$$
$$h_{f} = f \frac{L}{d} \frac{V^{2}}{2g} = 0.0143 \left(\frac{4.0}{0.007}\right) \frac{5^{2}}{2(9.81)} = 10.4 \text{ m} \text{ Ans. (a)}$$
$$\Delta p = \rho g h_{f} = (13550)(9.81)(10.4) = 1,380,000 \text{ } Pa = 1380 \text{ kPa} \text{ Ans. (b)}$$

P6.55 The reservoirs in Fig. P6.55 contain water at 20°C. If the pipe is smooth with L = 4500 m and d = 4 cm, what will the flow rate in m³/h be for $\Delta z = 100$ m?

Solution: For water at 20°C, take $\rho = 998 \text{ kg/m}^3$ and $\mu = 0.001 \text{ kg/m} \cdot \text{s}$. The energy equation from surface 1 to surface 2 gives

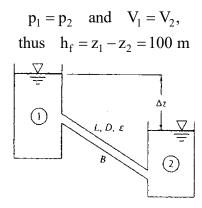


Fig. P6.55

Then 100 m = f
$$\left(\frac{4500}{0.04}\right) \frac{V^2}{2(9.81)}$$
, or $fV^2 \approx 0.01744$

Iterate with an initial guess of $f \approx 0.02$, calculating V and Re and improving the guess:

$$V \approx \left(\frac{0.01744}{0.02}\right)^{1/2} \approx 0.934 \ \frac{m}{s}, \quad \text{Re} \approx \frac{998(0.934)(0.04)}{0.001} \approx 37300, \quad f_{\text{smooth}} \approx 0.0224$$

$$V_{\text{better}} \approx \left(\frac{0.01744}{0.0224}\right)^{1/2} \approx 0.883 \ \frac{\text{m}}{\text{s}}, \quad \text{Re}_{\text{better}} \approx 35300, \quad \text{f}_{\text{better}} \approx 0.0226, \text{ etc....}$$

Alternately, one could, of course, use Excel. The above process converges to

$$f = 0.0227$$
, $Re = 35000$, $V = 0.877$ m/s, $Q \approx 0.0011$ m³/s ≈ 4.0 m³/h. Ans.