

## Flow Between Rotating Cylinders

An incompressible Newtonian liquid of density  $\rho$  and dynamic viscosity  $\mu$  is sheared between concentric cylinders with radius  $R_1$  (inner) and  $R_2$  (outer) rotating at angular velocity  $\omega_1$  and  $\omega_2$ . (a) Simplify the momentum equations and solve the differential equations to get the velocity  $u_\theta$  and pressure  $p$  profiles using the appropriate boundary conditions. (b) For what angular velocity must the outer cylinder rotate for stability assuming the inviscid stability criterion is sufficient, i.e.,  $d\gamma^2/dr > 0$  where  $\gamma = u_\theta r$ .

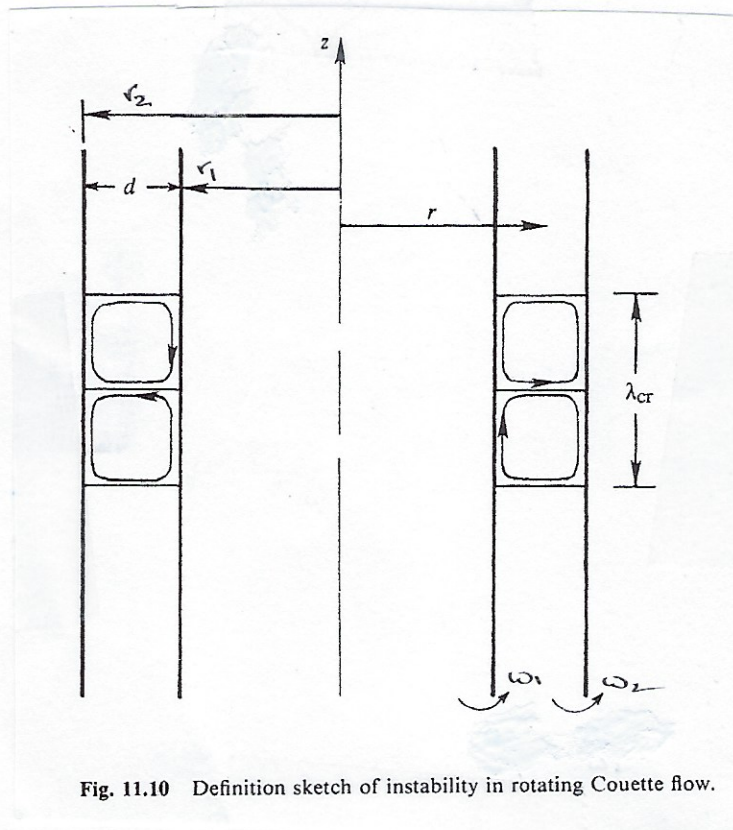


Fig. 11.10 Definition sketch of instability in rotating Couette flow.

$$(a) \quad \underline{v} = u_\theta(r) \hat{e}_\theta \quad p = p(r)$$

$$u_r = u_z = 0 \quad \frac{\partial}{\partial r} = \frac{\partial}{\partial \theta} = \frac{\partial}{\partial z} = 0$$

$$u_\theta(r_1) = r_1 \omega_1$$

$$u_\theta(r_2) = r_2 \omega_2$$

$$\text{Continuity: } \frac{1}{r} \frac{\partial}{\partial r} (r u_r) + \frac{1}{r} \frac{\partial}{\partial \theta} (u_\theta) + \frac{\partial}{\partial z} (u_z) = 0$$

$$\frac{1}{r} \frac{d}{dr} \left[ r \frac{du_\theta}{dr} \right] - \frac{u_\theta}{r^2} =$$

$$\frac{1}{r} \frac{du_\theta}{dr} + \frac{du_\theta}{dr} - \frac{u_\theta}{r^2}$$

$$\frac{d^2 u_\theta}{dr^2} + \frac{d}{dr} \left( \frac{u_\theta}{r} \right) = \frac{d}{dr} \left[ \frac{du_\theta}{dr} + \frac{u_\theta}{r} \right]$$

$$= \frac{d}{dr} \left[ \frac{1}{r} \frac{d}{dr} (r u_\theta) \right] \text{ momentum } r: -\frac{u_\theta^2}{r} = -\frac{1}{r} \frac{dp}{dr}$$

$$r u_r = \text{constant} \quad u_r = \frac{c}{r}$$

$$u_r(r_1) = u_r(r_2) = 0 \Rightarrow c = 0$$

outward force  
centrifugal  $\hat{=}$  balanced by  
 $p(r) \neq \frac{dp}{dr} = \frac{1}{r}$   $\uparrow$   
centripetal  
force

$$\text{circular Couette flow } \theta: 0 = \mu \left[ \nabla^2 u_\theta - \frac{u_\theta}{r^2} \right]$$

(1)  $u_\theta(r)$  driven

$$0 = \mu \left[ \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial u_\theta}{\partial r} \right) - \frac{u_\theta}{r^2} \right]$$

no slip satisfies

viscous diffusion

$$(2) \quad \frac{dp}{dr} = \frac{r \omega^2}{r}$$

$$0 = \mu \frac{d}{dr} \left[ \frac{1}{r} \frac{d}{dr} (r u_\theta) \right] = 2\mu A$$

$$u_\theta(r) = Ar + B/r$$

$Ar =$  rigid body rotation

$B/r =$  potential vortex

$$\frac{1}{r} \frac{dp}{dr} = \frac{u_\theta^2}{r}$$

$$u_\theta(r_1) = Ar_1 + B/r_1 = r_1 \omega_1$$

$$u_\theta(r_2) = Ar_2 + B/r_2 = r_2 \omega_2$$

$$A = (r_2^2 \omega_2 - r_1^2 \omega_1) / (r_2^2 - r_1^2)$$

$$B = r_1^2 r_2^2 (\omega_1 - \omega_2) / (r_2^2 - r_1^2)$$

$$p(r)/\rho = \frac{Ar^2 r^2}{2} + 2AB \ln r - \frac{B^2}{4r^4} + c$$

$$p(r=r_1, r_2) \Rightarrow c$$

$$u_\theta(r) = Ar + B/r$$

(2) rigid body rotation :  $\omega_1 = 0, r_1 = 0$

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$$u_\theta(r) = \omega_2 r$$

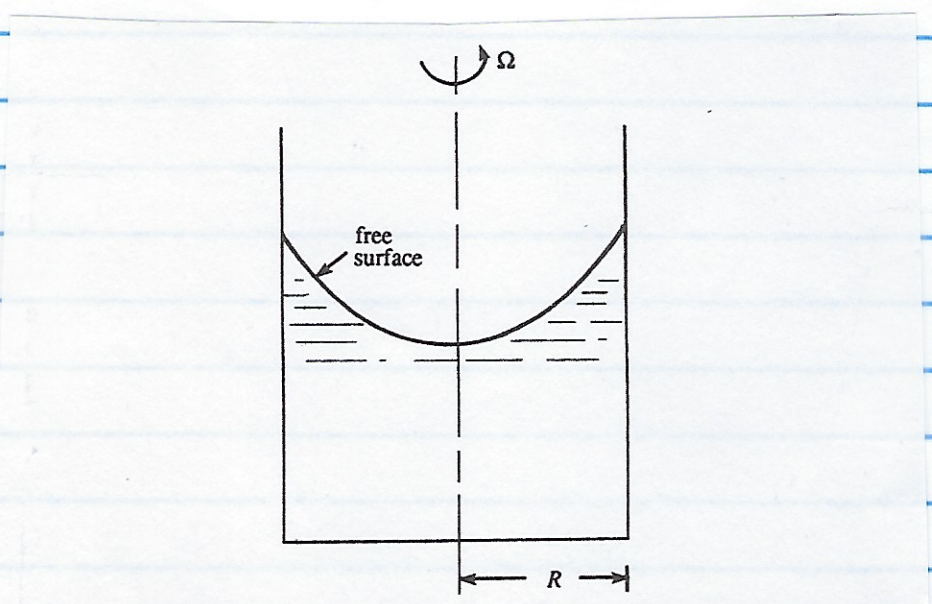


Figure 9.8 Steady rotation of a tank containing viscous fluid. The shape of the free surface is also indicated.

(2) potential vortex:  $\omega_2 = 0, r_2 \rightarrow \infty$

$$u_\theta(r) = \frac{r_1^2 \omega_1}{r}$$

equivalent potential flow vortex driven by inner rotating cylinder with no-slip condition, as per chapter 8

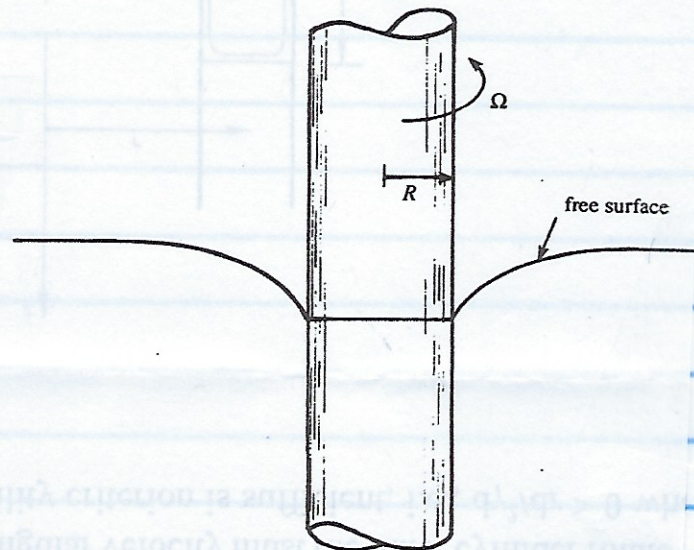


Figure 9.7 Rotation of a solid cylinder of radius  $R$  in an infinite body of viscous fluid. The flow field is viscous but irrotational.

8.14 A tornado may be modeled as the circulating flow shown in Fig. P8.14, with  $v_r = v_z = 0$  and  $v_\theta(r)$  such that

$$v_\theta = \begin{cases} \omega r & r \leq R \\ \frac{\omega R^2}{r} & r > R \end{cases}$$

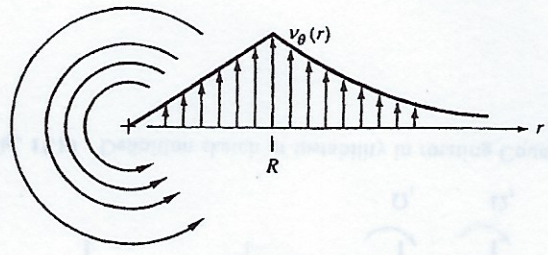
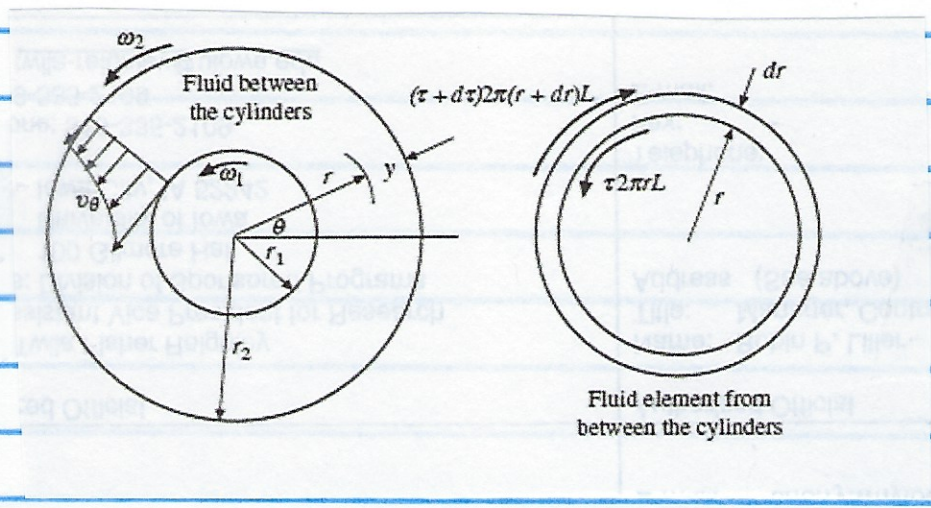


Fig. P8.14

Determine whether this flow pattern is irrotational in either the inner or outer region. Using the  $r$ -momentum equation (D.5) of App. D, determine the pressure distribution  $p(r)$  in the tornado, assuming  $p = p_\infty$  as  $r \rightarrow \infty$ . Find the location and magnitude of the lowest pressure.

$$u_\theta(r) = Ar + B/r$$



1888

Rayleigh's rotating inviscid flow stability criterion on circular shearlines

$$\Theta \text{ momentum } \times r = r \left[ \frac{\partial u_\theta}{\partial t} + 2\omega r \frac{\partial u_\theta}{\partial r} + \frac{u_\theta \omega}{r} + u_z \frac{\partial u_\theta}{\partial z} \right] = 0$$

$$= \frac{D\delta}{Dt} = \frac{\partial \delta}{\partial t} + \underline{v} \cdot \nabla \delta = 0 \quad \delta = r u_\theta$$

i.e. axisymmetric disturbance must maintain  $\delta = \text{constant} = \text{reduced circulation}$

circulation definition  $\Gamma = \oint \underline{u} \cdot d\underline{x} = \int_0^{2\pi} u_\theta(r) r d\theta$

$$\Gamma / 2\pi = \delta = 2\pi r u_\theta$$

$$KE = \frac{1}{2} \rho u_\theta^2 = \frac{1}{2} \rho \delta^2 / r^2 = 2\pi r^2 \omega \quad u_\theta = r\omega$$

before disturbance = exchange

$$KE_A = \rho/2 \left[ \left( \frac{\delta_1}{r_1} \right)^2 + \left( \frac{\delta_2}{r_2} \right)^2 \right]$$

fluid rings at  $r_1$  and  $r_2$  where  $r_1, r_2$  arbitrary

after

$$KE_B = \rho/2 \left[ \left( \frac{\delta_1}{r_2} \right)^2 + \left( \frac{\delta_2}{r_1} \right)^2 \right]$$

but  $r_2 > r_1$

$$\Delta KE = KE_B - KE_A = \frac{1}{2} \rho (\delta_2^2 - \delta_1^2) (r_1^{-2} - r_2^{-2})$$

$\Delta E > 0, \delta_2^2 > \delta_1^2$  Stable  
 ie requires E for exchange  
 $\Delta E < 0, \delta_2^2 < \delta_1^2$  unstable ie E released at disturbance can grow: centrifugal force > centripetal force  
 $\frac{d\delta^2}{dt} > 0$  stability  
 $(r_2 u_{\theta 2})^2 > (r_1 u_{\theta 1})^2$   
 $(r_2^2 \omega_2)^2 > (r_1^2 \omega_1)^2$   
 $\omega_2 > \left(\frac{r_1}{r_2}\right)^2 \omega_1$   
 $r^2 \omega$  must increase radially for stability

1923 Taylor rotating viscous flow stability criterion

Taylor Vortices

axisymmetric  $r, \theta, z$  NS equations with  
 $\underline{v} = \underline{\bar{v}} + \underline{u}$  = mean + disturbance  
 $P = \bar{P} + p$   
 mean solution given  $u_{\theta}(r) = Ar + B/r$   
 Substitute  $\underline{v}, P$  into NS, linearize  
 Assume disturbance  $e^{\alpha z + i k z}$  normal modes  
 Narrow gap solution

$$Ta = \frac{r_1 (r_2 - r_1)^3 (\omega_1^2 - \omega_2^2)}{v^2}$$

= centrifugal outward force / viscous force

$Ta_{crit} = 1708 \quad 0 \leq \omega_2/\omega_1 \leq 1$   
 $\lambda_{crit} = 2\pi d / k_{crit}$   
 $k_{crit} = 3.12 \Rightarrow \lambda_{crit} \sim 2d$

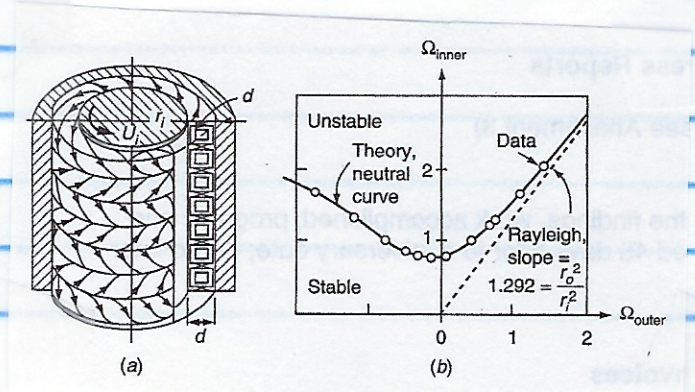


FIGURE 5-22 Theory and experiment by Taylor (1923) for the instability of Couette flow between rotating cylinders: (a) Taylor vortices; (b) theory and experiment for  $r_o = 4.035$  cm,  $r_i = 3.55$  cm.