Momentum and

quiescent fluid, $u_{\infty}=0$

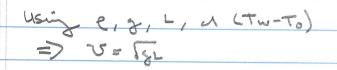
gravity

thermal boundary layers, $\hat{o} = \hat{o}$,

P5.46 If a vertical wall at temperature $T_{\rm w}$ is surrounded by a fluid at temperature $T_{\rm o}$, a convection boundary layer flow will form. For laminar flow, the momentum equation is

$$\rho(u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}) = \rho\beta(T - T_o)g + \mu\frac{\partial^2 u}{\partial y^2}$$

to be solved, along with continuity and energy, for (u, v, T) with appropriate boundary conditions. The quantity β is the thermal expansion coefficient of the fluid. Use ρ , g, L, and $(T_w - T_o)$ to nondimensionalize this equation. Note that there is no "stream" velocity in this type of flow.





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4-13.3 Free Convection along a Vertical Isothermal Plate

For a vertical plate with $g_x = g$, let us assume constant T_w . If we ignore the anomalous case of water near freezing, where β may be negative, all common fluids have low density at a hot wall. Buoyant motion and free convection are both upward along a hot vertical plate, and the leading edge x = 0 starts at the bottom. For a cold plate, buoyancy is downward and x = 0 is located at the top of the plate. The coordinate y is normal to the plate.

Since the local Grashof number Gr_x plays the role of Re_x^2 in buoyant motion, we can guess (correctly) that the boundary-layer thickness δ/x will be proportional to $Gr_x^{1/4}$. Indeed, the "scale analysis" in the text by Bejan (1994) predicts that δ will be proportional to $x^{1/4}$. For vertical plate flow, velocity and thickness scales are prescribed by Schmidt et al. (1930) in an assortment of similarity variables:

$$\eta = \left(\frac{Gr_x}{4}\right)^{1/4} \frac{y}{x} \quad Gr_x = \frac{\beta g(T_w - T_\infty)x^3}{\nu^2} \quad u = 2\sqrt{x\beta g(T_w - T_\infty)}f' \quad v = \left[\frac{\beta g(T_w - T_\infty)\nu^2}{4x}\right]^{1/4} (\eta f' - 3f) \quad \Theta = \frac{T - T_\infty}{T_w - T_\infty} (4-259)$$

The reader can verify that u and v satisfy continuity and that these variables will reduce momentum and energy relations to the two coupled nonlinear ordinary differential equations

$$f''' + 3ff'' - 2f'^2 + \Theta = 0$$
 and $\Theta'' + 3Prf\Theta' = 0$ (4-260)

subject to the boundary conditions

$$f(0) = f'(0) = f'(\infty) = 0$$
 and $\Theta(0) = 1$ $\Theta(\infty) = 0$ (4-261)

Note that Eqs. (4-260) are coupled and must be solved simultaneously, which is always the case in free-convection problems. Since no analytic solution is known, numerical integration is necessary. There are two unknown initial values at the wall. One must find the proper values of f''(0) and $\Theta'(0)$, which cause the velocity and temperature to vanish for large η .

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$$\rho(u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}) = \rho\beta(T - T_o)g + \mu\frac{\partial^2 u}{\partial v^2}$$

to be solved, along with continuity and energy, for (u, v, T) with appropriate boundary conditions. The quantity β is the thermal expansion coefficient of the fluid. Use ρ , g, L, and $(T_w - T_0)$ to nondimensionalize this equation. Note that there is no "stream" velocity in this type of flow.

Solution: For the given constants used to define dimensionless variables, there is only one pairing which will give a velocity unit: $(gL)^{1/2}$. Here are the writer's dimensionless variables:

$$u^* = \frac{u}{\sqrt{gL}} \ ; \ v^* = \frac{v}{\sqrt{gL}} \ ; \ x^* = \frac{x}{L} \ ; \ y^* = \frac{y}{L} \ ; \ T^* = \frac{T - T_o}{T_w - T_o}$$

Substitute into the momentum equation above and clean up so all terms are dimensionless:

$$\begin{split} &\rho(u*\frac{\partial u*gL}{\partial x*L})+\rho(v*\frac{\partial u*gL}{\partial y*L})=\rho\beta g(T_w-T_o)T*+\mu\frac{\partial^2 u*\sqrt{gL}}{\partial y*^2}\\ &\text{or}: \qquad u*\frac{\partial u*}{\partial x*}+v*\frac{\partial u*}{\partial y*}=[\beta(T_w-T_o)]T*+[\frac{\mu}{\rho L\sqrt{gL}}]\frac{\partial^2 u*}{\partial y*^2} \quad \textit{Ans}. \end{split}$$

There are two dimensionless parameters: $\beta(T_w-T_o)$ and $\mu/[\rho L\sqrt{gL}]$. Neither has a name, to the writer's knowledge, because a much cleverer analysis would result in only a single dimensionless parameter, the *Grashof number*, $g\beta(T_w-T_o)L^3/v^2$. (See, for example, White, *Viscous Fluid Flow*, 3rd edition, Section 4-14.3, page 323.)